

Aspirin production

Chemical reaction

salicylic acid + acetic anhydride + phosphoric acid
 (SA, \$1.33/lbm) (AAH, \$0.49/lbm) (PA, \$0.34/lbm)

→ acetylsalicylic acid + acetic acid + phosphoric acid.

$k_r = 0.55^{-1}$
 $H_r = -85600 \text{ J/mol}$ (ASA, \$3.97/lbm) (AA, \$0.013/lbm) (PA, \$0.34/lbm)

Cost information

(cooling water: \$0.03/1000 gal)
 (electricity: \$0.05/kw.hr)

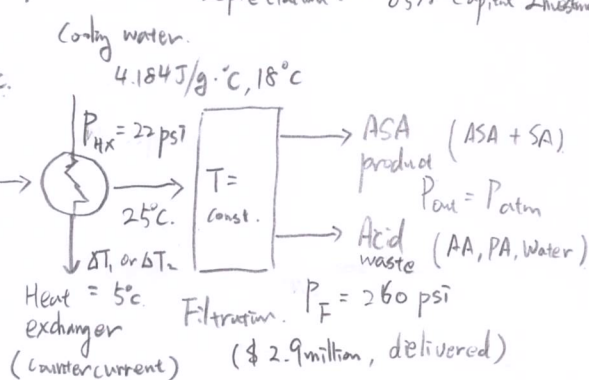
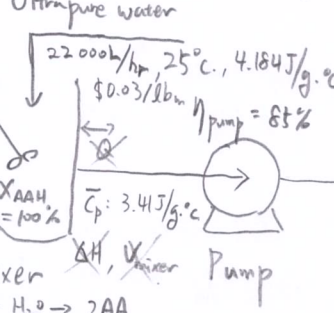
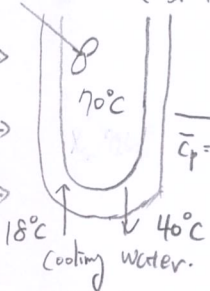
Operating cost: 1.55 (feed + cooling water + electricity)

Tax rate: $\phi = 0.35$ • Depreciation: 85% Capital Investment/10 year

Inlet

1. SA 2000 kg/hr
2. AAH 5000 L/hr
3. PA 1250 L/hr

Reactor ($X_{SA} = 99.5\%$)



(Ans 1)

1. Material balances (Ans 2)

1.1. Reactor

Stoichiometry

SA: $\dot{n}_{SA,in} = \dot{n}_{SA,out} + r_{c,SA}$

AAH: $\dot{n}_{AAH,in} = \dot{n}_{AAH,out} + r_{c,AAH}$

PA: $\dot{n}_{PA,in} = \dot{n}_{PA,out}$

ASA: $r_{f,ASA} = \dot{n}_{ASA,out}$

AA: $r_{f,AA} = \dot{n}_{AA,out}$

$r_{c,AAH} / r_{c,SA} = 1$, $r_{c,AAH} = 14.41 \text{ kg/ml/hr}$

$r_{f,SA} / r_{c,SA} = 1$, $r_{f,SA} = 14.41 \text{ kg/ml/hr}$

$r_{f,AA} / r_{c,SA} = 1$, $r_{f,AA} = 14.41 \text{ kg/ml/hr}$

$r_{c,SA} = 0.995 \cdot \dot{n}_{SA,in} = 0.995 \frac{\dot{m}_{SA,in}}{MW_{SA}} = 0.995 \cdot \frac{2000 \text{ kg/hr}}{138.1 \text{ kg/kgml}} = 14.41 \text{ kg/ml/hr}$

$\dot{n}_{SA,out} = \dot{n}_{SA,in} - r_{c,SA} = \frac{2000 \text{ kg/hr}}{138.1 \text{ kg/kgml}} - 14.41 \text{ kg/ml/hr} = 0.07 \text{ kg/ml/hr} \text{ (9.67 kg/hr)}$

$\dot{n}_{AAH,out} = \dot{n}_{AAH,in} - r_{c,AAH} = \frac{\rho_{AAH} \cdot \dot{V}_{AAH,in}}{MW_{AAH}} - r_{c,AAH} = \frac{1.08 \text{ g/cm}^3 \cdot 5000 \text{ L/hr}}{102.1 \text{ kg/kgml}} - 14.41 \text{ kg/ml/hr} = 38.48 \text{ kg/ml/hr} \text{ (3928.81 kg/hr)}$

$\dot{n}_{PA,out} = \dot{n}_{PA,in} = \frac{\rho_{PA} \cdot \dot{V}_{PA}}{MW_{PA}} = \frac{1.66 \text{ g/cm}^3 \cdot 1250 \text{ L/hr}}{98 \text{ kg/kgml}} = 21.43 \text{ kg/ml/hr} \text{ (2100.14 kg/hr)}$

$\dot{n}_{ASA,out} = r_{f,ASA} = 14.41 \text{ kg/ml/hr} \text{ (2596.68 kg/hr)}$, $\dot{n}_{AA,out} = r_{f,AA} = 14.41 \text{ kg/ml/hr} \text{ (866.04 kg/hr)}$

$\therefore \dot{m}_{reactor,out} = 9.67 + 3928.81 + 2100.14 + 2596.68 + 866.04 = 9501.34 \text{ kg/hr}$

SA AAH PA ASA AA

1.2 Mixer

Stoichiometry

$$\text{AAH} : \dot{n}_{\text{AAH},in} = \dot{n}_{\text{AAH},out} + r_{c,AAH}$$

$$\text{Water} : \dot{n}_{w,in} = \dot{n}_{w,out} + r_{c,w}$$

$$\text{AA} : \dot{n}_{AA,in} + r_{f,AA} = \dot{n}_{AA,out}$$

$$r_{c,w} / r_{c,AAH} = 1, \quad r_{c,w} = 38.48 \text{ kgmol/hr}$$

$$r_{f,AA} / r_{c,AAH} = 2, \quad r_{f,AA} = 76.96 \text{ kgmol/hr}$$

$$r_{c,AAH} = 1.0 \times \dot{n}_{\text{AAH},in} = 38.48 \text{ kgmol/hr}$$

$$\dot{n}_{w,out} = \dot{n}_{w,in} - r_{c,w} = \frac{\rho_w \dot{V}_{w,in}}{MW_w} - r_{c,w} = \frac{1 \text{ g/cm}^3 \cdot 22000 \text{ L/hr}}{18 \text{ kg/kgmol}} - 38.48 \text{ kgmol/hr} = 1183.74 \text{ kgmol/hr}$$

$$(21307.32 \text{ kg/hr})$$

$$\dot{n}_{AA,out} = \dot{n}_{AA,in} + r_{f,AA} = 14.41 + 76.96 = 91.37 \text{ kgmol/hr} (5491.34 \text{ kg/hr})$$

$$\dot{m}_{\text{mixer},out} = \dot{m}_{\text{reactor},out} + \dot{m}_{w,in} = 9501.34 + 22000 = 31501.34 \text{ kg/hr}$$

1.3 Filtration

ASA product. $\left\{ \begin{array}{l} \text{ASA} : 14.41 \text{ kgmol/hr} \\ \text{SA} : 0.09 \text{ kgmol/hr} \end{array} \right.$

Acid waste : $\left\{ \begin{array}{l} \text{AA} : 91.37 \text{ kgmol/hr} \\ \text{PA} : 21.43 \text{ kgmol/hr} \\ \text{Water} : 1183.74 \text{ kgmol/hr} \end{array} \right.$

2. Equipment sizing

2.1 Reactor

$$r_{c,SA} = k_r \cdot C_{SA,out} \cdot V_r = k_r \cdot \frac{\dot{n}_{SA,out}}{\dot{V}_{out}} \cdot V_r = k_r \cdot \dot{n}_{SA,out} \cdot \frac{P_{out}}{\dot{m}_{out}} \cdot V_r$$

$$\therefore V_r = \frac{r_{c,SA} \cdot \dot{m}_{out}}{k_r \cdot \dot{n}_{SA,out} \cdot P_{out}} = \frac{14.41 \text{ kgmol/hr} \cdot 9501.34 \text{ kg/hr}}{0.557 \cdot 0.09 \text{ kgmol/hr} \cdot 1.2 \text{ g/cm}^3} = 905.5 \text{ L} = 239.2 \text{ gal} \quad (\text{Ans 5, 9})$$

2.2 Pumps

$$\frac{P_2 - P_1}{\rho} + \frac{1}{2} (dV_{avg,2}^2 - dV_{avg,1}^2) + g(z_2 - z_1) = W_s - W_f$$

Same diameter same level

$$W_s = \frac{P_2 - P_1}{\rho} = \frac{20 \text{ psi} + 260 \text{ psi}}{1.2 \text{ g/cm}^3} \cdot \left(\frac{1 \text{ g/cm}^3}{62.43 \text{ lbm/ft}^3} \right) \cdot \left(\frac{\text{lb}_f/\text{in}^2}{1 \text{ psi}} \right) \cdot \left(\frac{144 \text{ in}^2}{\text{ft}^2} \right) \cdot \left(\frac{1 \text{ hp}}{550 \text{ ft} \cdot \text{lbm/s}} \right) = 0.986 \frac{\text{hp}}{\text{lbm/s}}$$

$$W = \dot{m}_{\text{mixer},out} \cdot W_s = 31501.34 \text{ kg/hr} \cdot 0.986 \frac{\text{hp}}{\text{lbm/s}} \cdot \frac{1 \text{ hr}}{3600 \text{ s}} \cdot \frac{2.205 \text{ lbm}}{1 \text{ kg}} = 19.02 \text{ hp}$$

$$\therefore \text{Power to operating pump} = \frac{\text{Power delivered to the fluid}}{\text{efficiency}} = \frac{19.02 \text{ hp}}{0.85} = 22.38 \text{ hp} \quad (\text{Ans 6, 9})$$

3. Energy balance (Ans 3)

3.1. Reactor

$$\dot{Q}_{\text{reactor}} = \Delta \hat{H}_{\text{reaction}} \cdot r_{c,SA} = -85800 \text{ J/gmol} \cdot 14.41 \text{ kgmol/hr} = -1.24 \times 10^9 \text{ J/hr}$$

$$\dot{Q}_{\text{cooling water}} = \dot{m}_{\text{cooling water}} \cdot \bar{C}_{p,w} \cdot (T_{\text{out}} - T_{\text{in}}) = 1.24 \times 10^9 \text{ J/hr} \quad (\text{Ans 9})$$

$$\dot{m}_{\text{cooling water}} = \frac{\dot{Q}_{\text{cooling water}}}{\bar{C}_{p,w} (T_{\text{out}} - T_{\text{in}})} = \frac{1.24 \times 10^9 \text{ J/hr}}{4.184 \text{ J/g} \cdot ^\circ\text{C} \cdot (40^\circ\text{C} - 18^\circ\text{C})} = 1.35 \times 10^7 \text{ g/hr} \quad (3550 \text{ gal/hr}) \quad (\text{Ans 4,9})$$

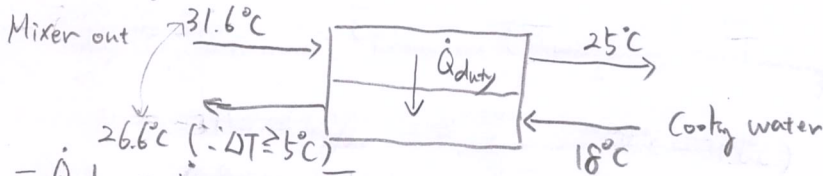
3.2. Mixer

$$\dot{Q}_{\text{reactor out}} = -\dot{Q}_{\text{ultrapure water}}$$

$$\dot{m}_{\text{reactor out}} \cdot \bar{C}_{p,\text{reactor out}} (T_f - T_{\text{reactor out}}) = -\dot{m}_{\text{ultrapure water}} \cdot \bar{C}_{p,w} (T_f - T_{\text{ultrapure water}})$$

$$T_f = \frac{9501.34 \text{ kg/hr} \cdot 1.67 \text{ J/g} \cdot ^\circ\text{C} \cdot 70^\circ\text{C} + 22000 \text{ kg/hr} \cdot 4.184 \text{ J/g} \cdot ^\circ\text{C} \cdot 25^\circ\text{C}}{9501.34 \text{ kg/hr} \cdot 1.67 \text{ J/g} \cdot ^\circ\text{C} + 22000 \text{ kg/hr} \cdot 4.184 \text{ J/g} \cdot ^\circ\text{C}} = 31.6^\circ\text{C}$$

3.3. Heat exchanger



$$\text{Hot: } -\dot{Q}_{\text{duty}} = \dot{m}_{\text{mixer out}} \cdot \bar{C}_{p,\text{mixer out}} \cdot (T_{\text{exchanger out}} - T_{\text{exchanger in}})$$

$$= 31501.34 \text{ kg/hr} \cdot 3.41 \text{ J/g} \cdot ^\circ\text{C} \cdot (25^\circ\text{C} - 31.6^\circ\text{C})$$

$$\therefore \dot{Q}_{\text{duty}} = 709000 \text{ kJ/hr} = 672000 \text{ Btu/hr} \quad (\text{Ans 9})$$

$$\text{Cold: } \dot{Q}_{\text{duty}} = \dot{m}_{\text{cooling water}} \cdot \bar{C}_{p,w} \cdot (T_{\text{out}} - T_{\text{in}}) = 709000 \text{ kJ/hr} \quad (\text{Ans 9})$$

$$\dot{m}_{\text{cooling water}} = \frac{709000 \text{ kJ/hr}}{4.184 \text{ J/g} \cdot ^\circ\text{C} \cdot (26.6 - 18^\circ\text{C})} = 19.7 \times 10^6 \text{ g/hr} \quad (5200 \text{ gal/hr}) \quad (\text{Ans 4,9})$$

$$\Delta T_1 = 5^\circ\text{C} = 9^\circ\text{F}, \quad \Delta T_2 = 7^\circ\text{C} = 12.6^\circ\text{F} \quad \therefore T_{\log \text{ mean}} = \frac{12.6 - 9}{\ln(12.6/9)} = 10.7^\circ\text{F}$$

$$U_0 = 50 \text{ Btu/hr} \cdot \text{ft}^2 \cdot ^\circ\text{F} \quad (\text{from Table 10.4})$$

$$\therefore A = \frac{\dot{Q}_{\text{duty}}}{U \cdot \Delta T_{\log \text{ mean}}} = \frac{672000 \text{ Btu/hr}}{50 \text{ Btu/hr} \cdot \text{ft}^2 \cdot ^\circ\text{F} \cdot 10.7^\circ\text{F}} = 1260 \text{ ft}^2 \quad (\text{Ans 7,9})$$

4. Economics

4.1. Capital investment

Equipment

$$\text{Reactor: } \frac{M\&S}{814} \cdot 47.0 (V/\text{gal})^{0.61} = \frac{1469}{814} \cdot 47.0 \cdot (239.2 \text{ gal})^{0.61} \doteq \$2400$$

$$\text{Heat exchanger: } \frac{1469}{814} \cdot 398 \cdot (1260 \text{ ft}^2)^{0.65} \doteq \$74400$$

$$\text{Pump: } \frac{1469}{814} \cdot 421 \cdot (139 \text{ gal/min})^{0.46} \doteq \$7300$$

$$\dot{V} = \frac{31501.34 \text{ kg/hr} \cdot \frac{1 \text{ m}^3}{1 \text{ kg}}}{\text{From mixer}} \doteq 139 \text{ gal/min.}$$

$\rho \approx \text{water.}$

$$\text{Filtration (delivery included): } \$2900000$$

$$\text{Total delivered cost} = (2400 + 74400 + 7300) \times 1.1 + 2900000 = \$2992500$$

$$\text{Capital Investment: } 6.0 \times \$2992500 = \$17955000$$

$$\text{Depreciation: } (0.85 \times \$17955000) / 10 = \$1526200 / \text{yr}$$

4.2 Operating cost

Feed

$$\text{SA: } \$1.33 / \text{lbm} \cdot 2000 \text{ kg/hr} = \$51380000 / \text{yr}$$

$$\text{AAH: } \$0.49 / \text{lbm} \cdot 5000 \text{ L/hr} \cdot P_{\text{AAH}} = \$51110000 / \text{yr}$$

$$\text{PA: } \$0.34 / \text{lbm} \cdot 1250 \text{ L/hr} \cdot P_{\text{PA}} = \$13790000 / \text{yr}$$

Ultrapure water: $\$0.03 / \text{lbm} \cdot 22000 \text{ L/hr} \cdot P_w = \$12750000 / \text{yr}$

Cooling water: $\$0.03 / 1000 \text{ gal} (3550 \text{ gal/hr} + 5200 \text{ gal/hr}) = \$2300 / \text{yr}$

Electricity: $\$0.05 / \text{kWh} \cdot 22.4 \text{ hp} = \$7300 / \text{yr}$

$$\therefore \text{operating cost} = 1.55 (\text{feed} + \text{water} + \text{electricity}) \doteq \$200000000 / \text{yr}$$

4.3 Sales

$$\text{ASA (aspirin): } \$3.97 / \text{lbm} \cdot 2600 \text{ kg/hr} = \$199910000 / \text{yr}$$

$$\text{Acid waste: } \$0.013 / \text{lbm} \cdot 28900 \text{ kg/hr} = \$7260000 / \text{yr}$$

(AA) (31500 - 2600)

$$\left. \begin{array}{l} \text{ASA (aspirin)} \\ \text{Acid waste} \end{array} \right\} \$207170000 / \text{yr}$$

$$4.4 \text{ Gross profit} = \text{sales} - \text{operating cost} - \text{depreciation}$$

$$= \$207170000 / \text{yr} - \$200000000 / \text{yr} - \$1526200 / \text{yr}$$

$$= \$5643800 / \text{yr}$$

$$4.5 \text{ NAPAT} = \$5643800 / \text{yr} \cdot (1 - 0.35) = \$3668500 / \text{yr}$$

$$4.6 \text{ ROI: } \frac{\text{NAPAT}}{\text{Capital investment}} = \frac{\$3668500 / \text{yr}}{\$17955000} = 20.4\% \quad (\text{Ans 10})$$

↳ (Ans 11).